

# Energy Balance for a Moving Defect in a Peridynamic Solid

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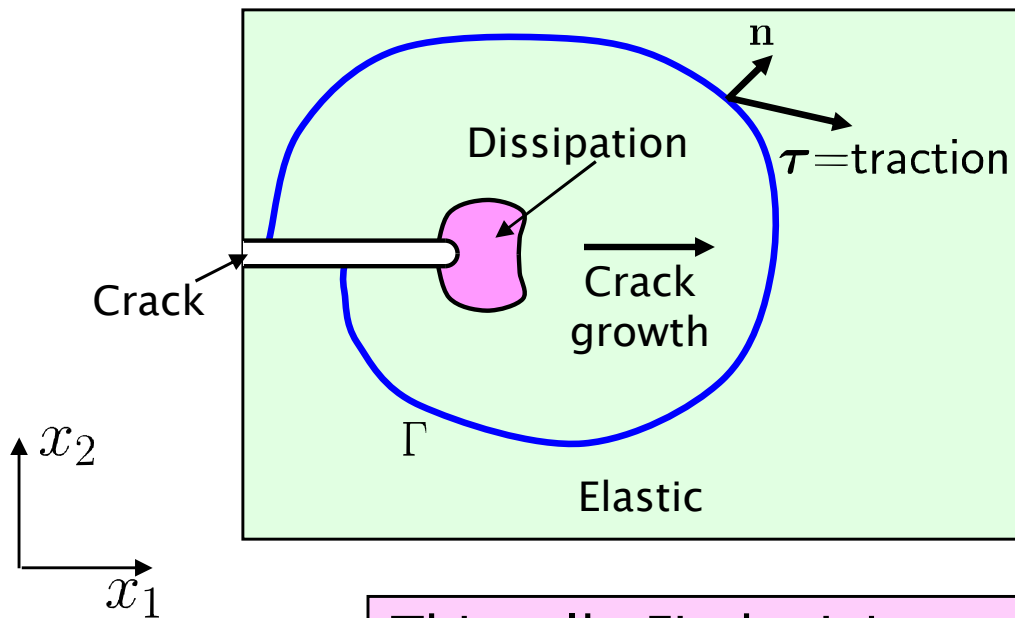


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# Energy flow into a defect: Results from the local theory

- The energy dissipated by a moving defect can be obtained from the elastic fields far from the defect.
  - Don't need to know all the small-scale details.
- Eshelby (1956): 3D energy-momentum tensor and its surface integral.
- Rice (1968): 2D J-integral and its relation to plastic flow.
- Knowles & Sternberg (1972): Obtained J-integral from Noether's theorem.



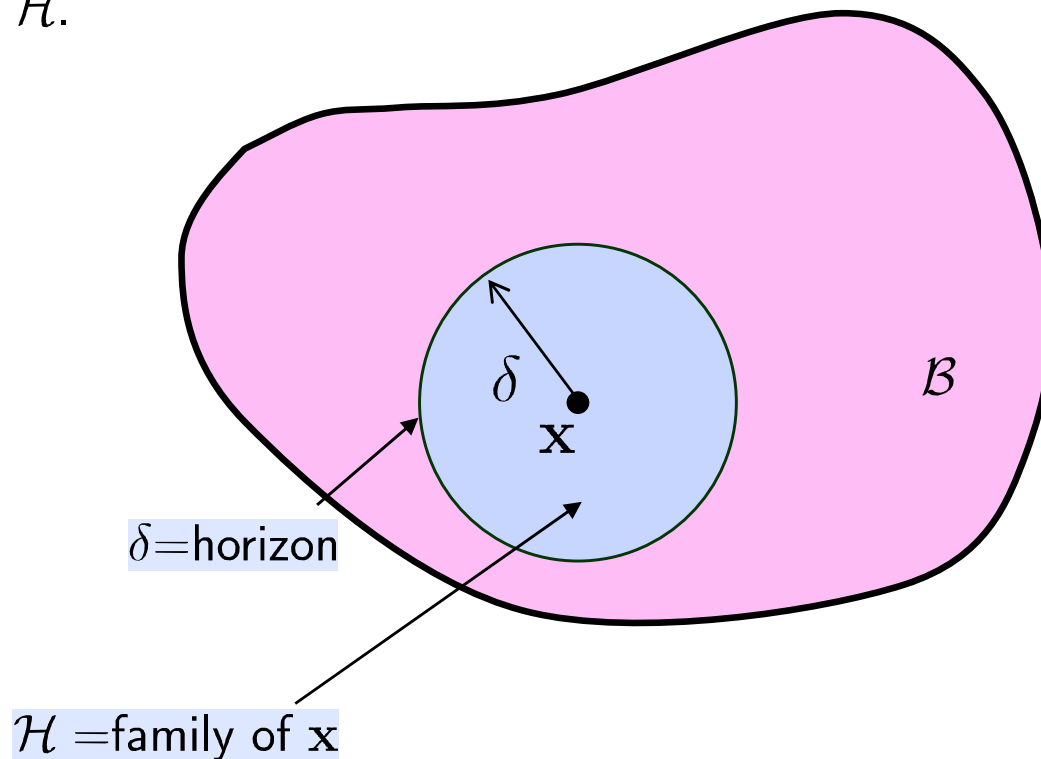
$$J = \int_{\Gamma} \left[ W n_2 - \boldsymbol{\tau} \cdot \frac{\partial \mathbf{u}}{\partial x_1} \right] d\ell$$

= energy per unit crack area  
= "driving force" on defect

This talk: Find a J-integral in peridynamics.

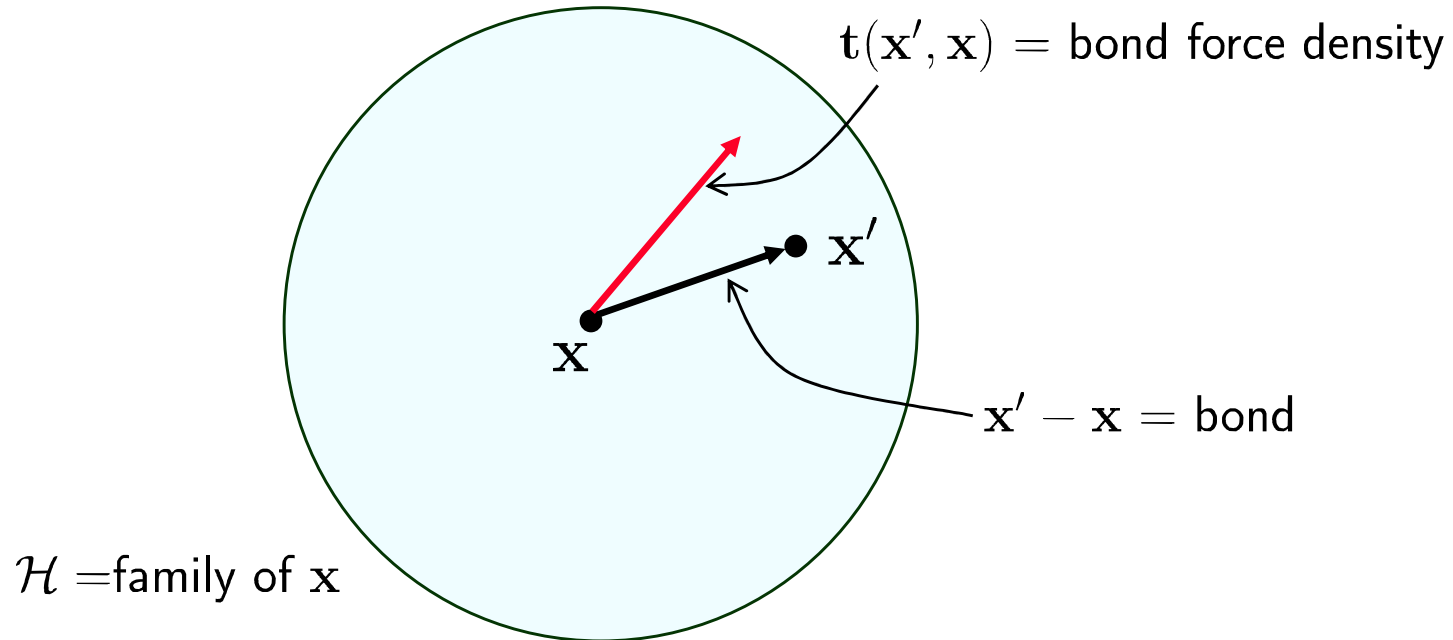
# Peridynamics basics: Horizon and family

- Any point  $\mathbf{x}$  interacts directly with other points within a finite distance  $\delta$  called the “horizon.”
- The material within a distance  $\delta$  of  $\mathbf{x}$  is called the “family” of  $\mathbf{x}$ ,  $\mathcal{H}$ .



# Bond forces

- A force density  $\mathbf{t}(\mathbf{x}', \mathbf{x})$  is associated with each bond in the family of  $\mathbf{x}$ .
- Dimensions of  $\mathbf{t}$  are force/volume<sup>2</sup>.
- $\mathbf{t}$  is not necessarily parallel to the deformed bond.



# Bond forces are determined by the collective deformation of the family

- The *deformation state*  $\underline{\mathbf{Y}}$  is the function that maps bonds to their deformed images.

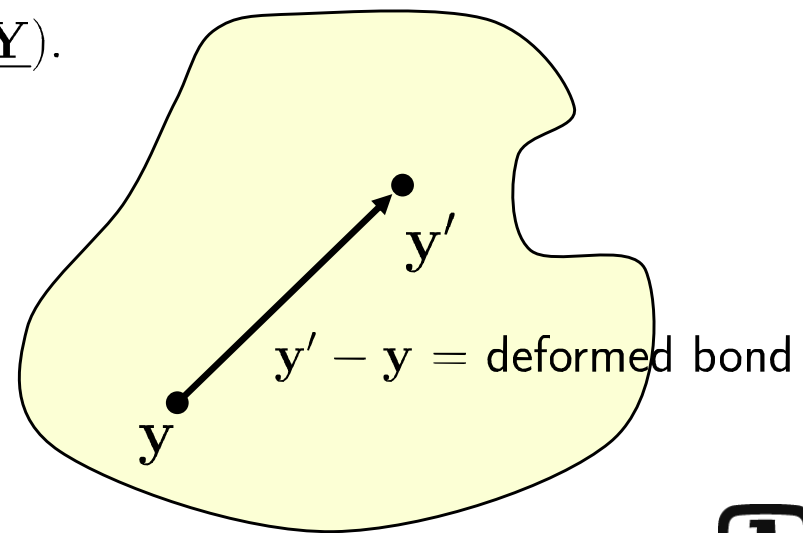
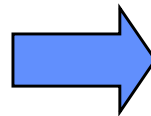
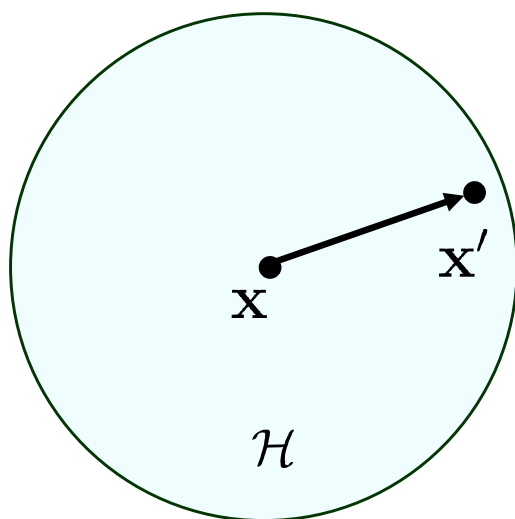
$$\mathbf{y}' - \mathbf{y} = \underline{\mathbf{Y}}\langle \mathbf{x}' - \mathbf{x} \rangle.$$

- The *force state*  $\underline{\mathbf{T}}$  is the function that maps bonds to bond forces.

$$\mathbf{t}(\mathbf{x}', \mathbf{x}) = \underline{\mathbf{T}}\langle \mathbf{x}' - \mathbf{x} \rangle.$$

- The *constitutive model*  $\hat{\underline{\mathbf{T}}}$  relates  $\underline{\mathbf{T}}$  and  $\underline{\mathbf{Y}}$ :

$$\underline{\mathbf{T}} = \hat{\underline{\mathbf{T}}}(\underline{\mathbf{Y}}).$$

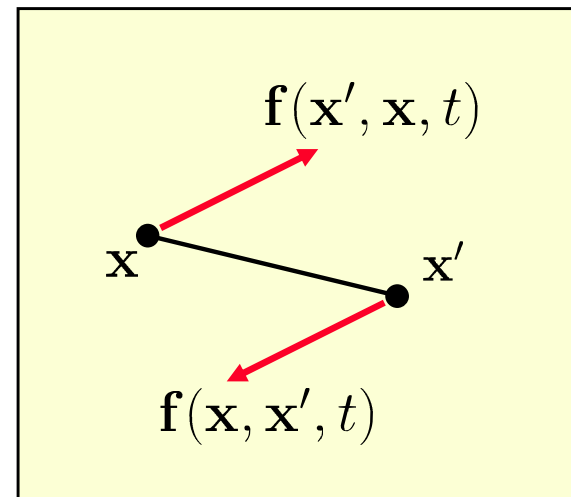
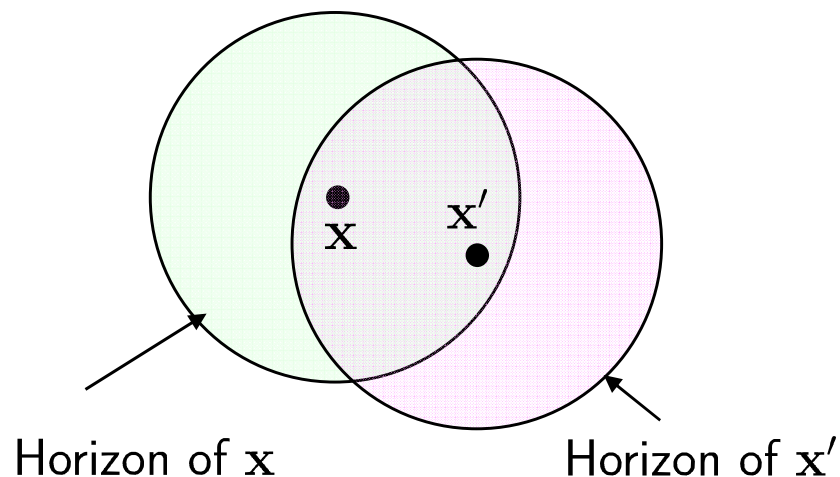


# Peridynamic equation of motion

- At any point  $\mathbf{x}$  in the reference configuration of the body  $\mathcal{B}$ :

$$\rho(\mathbf{x})\ddot{\mathbf{y}}(\mathbf{x}, t) = \int_{\mathcal{H}} (\mathbf{t}(\mathbf{x}', \mathbf{x}, t) - \mathbf{t}(\mathbf{x}, \mathbf{x}', t)) dV' + \mathbf{b}(\mathbf{x}, t)$$

Dual force density  $\mathbf{f}(\mathbf{x}', \mathbf{x}, t)$





# Energy balance at a point

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- First law expression for peridynamics:

$$\dot{\varepsilon} = \underline{\mathbf{T}} \bullet \underline{\dot{\mathbf{Y}}} + h + r$$

where  $\varepsilon$ =internal energy density,  $h$ =heat transport rate,  
 $r$ =energy source rate.

- Dot product represents, at any  $\mathbf{x}$ ,

$$\underline{\mathbf{T}} \bullet \underline{\dot{\mathbf{Y}}} = \int_{\mathcal{H}} \mathbf{t}(\mathbf{x}', \mathbf{x}, t) \cdot (\mathbf{v}(\mathbf{x}', t) - \mathbf{v}(\mathbf{x}, t)) dV'$$

- Assume an adiabatic, source-free process:  $h = r = 0$ .
- The term  $\underline{\mathbf{T}} \bullet \underline{\dot{\mathbf{Y}}}$  is called the *absorbed power density* (peridynamic version of stress power  $\boldsymbol{\sigma} \cdot \dot{\mathbf{F}}$ ).

# Energy balance for a subregion

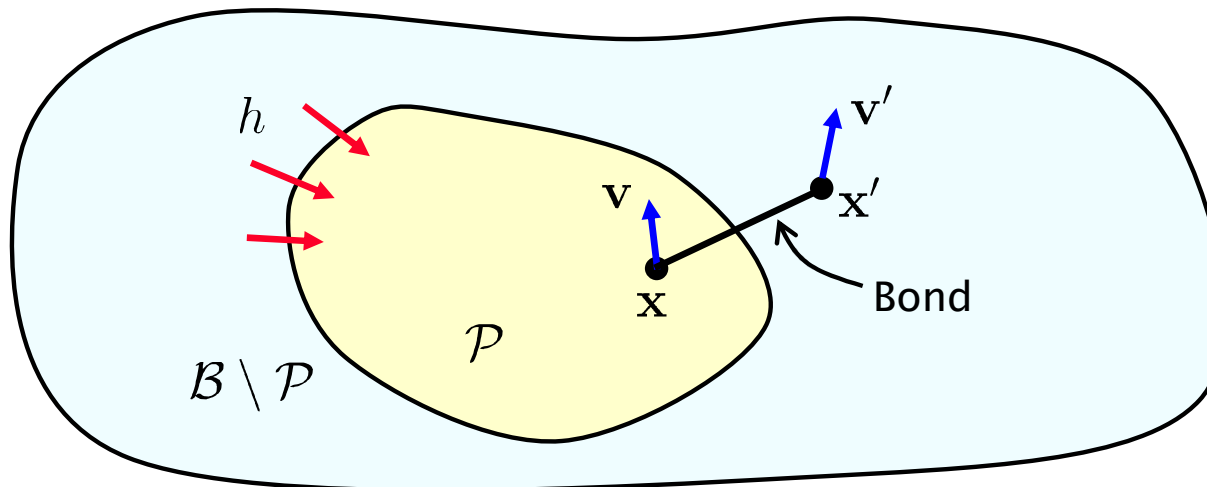
- Global first law expression in peridynamics for a subregion  $\mathcal{P} \subset \mathcal{B}$ :

$$\frac{d}{dt} \int_{\mathcal{P}} \left( \varepsilon + \frac{\rho \mathbf{v} \cdot \mathbf{v}}{2} \right) dV = \int_{\mathcal{P}} \int_{\mathcal{B} \setminus \mathcal{P}} (\mathbf{t} \cdot \mathbf{v}' - \mathbf{t}' \cdot \mathbf{v}) dV' dV + \int_{\mathcal{P}} (h + r) dV + \int_{\mathcal{P}} \mathbf{b} \cdot \mathbf{v} dV$$

where following short notation is used:

$$\mathbf{t} = \mathbf{t}(\mathbf{x}', \mathbf{x}, t), \quad \mathbf{v} = \mathbf{v}(\mathbf{x}, t)$$

$$\mathbf{t}' = \mathbf{t}(\mathbf{x}, \mathbf{x}', t), \quad \mathbf{v}' = \mathbf{v}(\mathbf{x}', t).$$







# Free energy and the force state

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- Free energy is defined by

$$\psi = \varepsilon - \theta \eta$$

where  $\theta$ =temperature,  $\eta$ =entropy density.

- Assume  $\psi$  has the following dependencies:

$$\psi(\underline{\mathbf{Y}}, \theta, \underline{\phi})$$

where  $\underline{\phi}$  is the *damage state* (next slide).

- Can show by Coleman-Noll procedure that

$$\underline{\mathbf{T}} = \psi_{\underline{\mathbf{Y}}}$$

where  $\psi_{\underline{\mathbf{Y}}}$  is the Fréchet derivative of  $\psi$  with respect to  $\underline{\mathbf{Y}}$ .

# Damage state

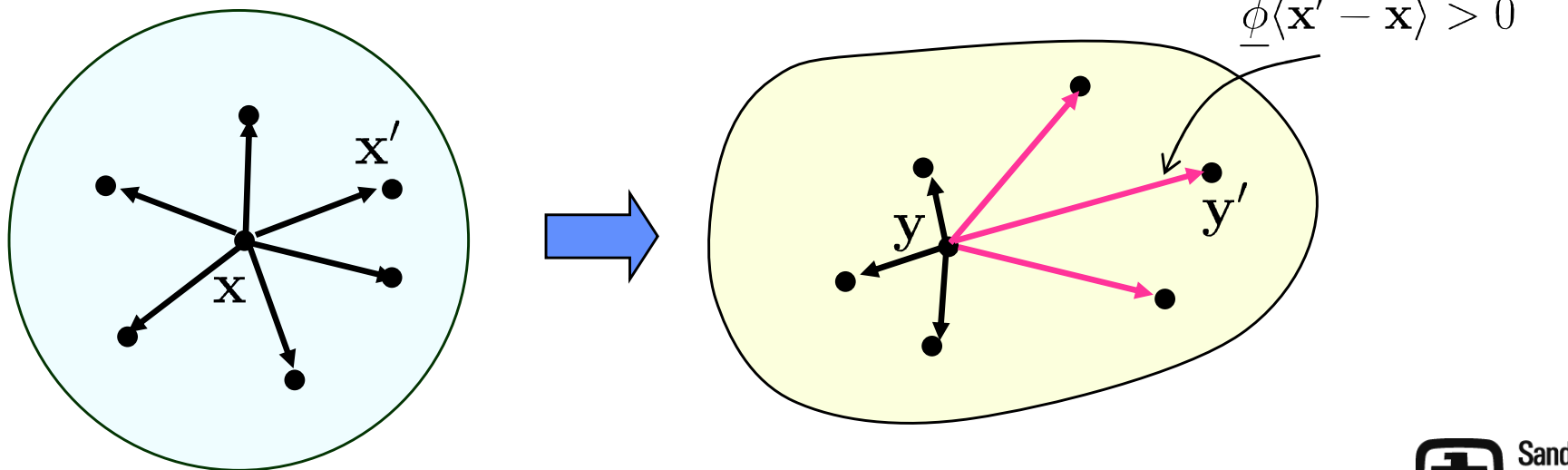
- The damage state increases monotonically for each bond  $\mathbf{x}' - \mathbf{x}$ :

$$\dot{\underline{\phi}}\langle \mathbf{x}' - \mathbf{x} \rangle \geq 0, \quad 0 \leq \underline{\phi}\langle \mathbf{x}' - \mathbf{x} \rangle \leq 1.$$

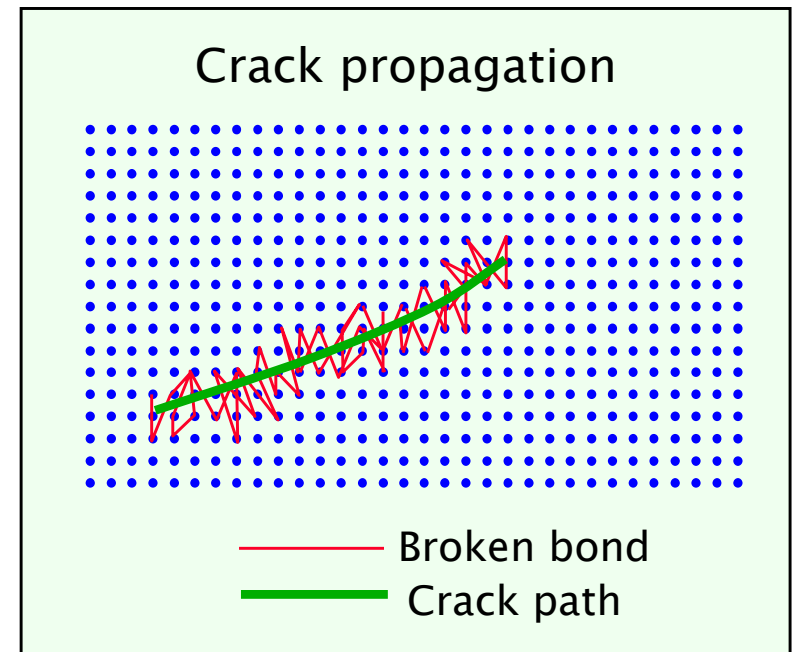
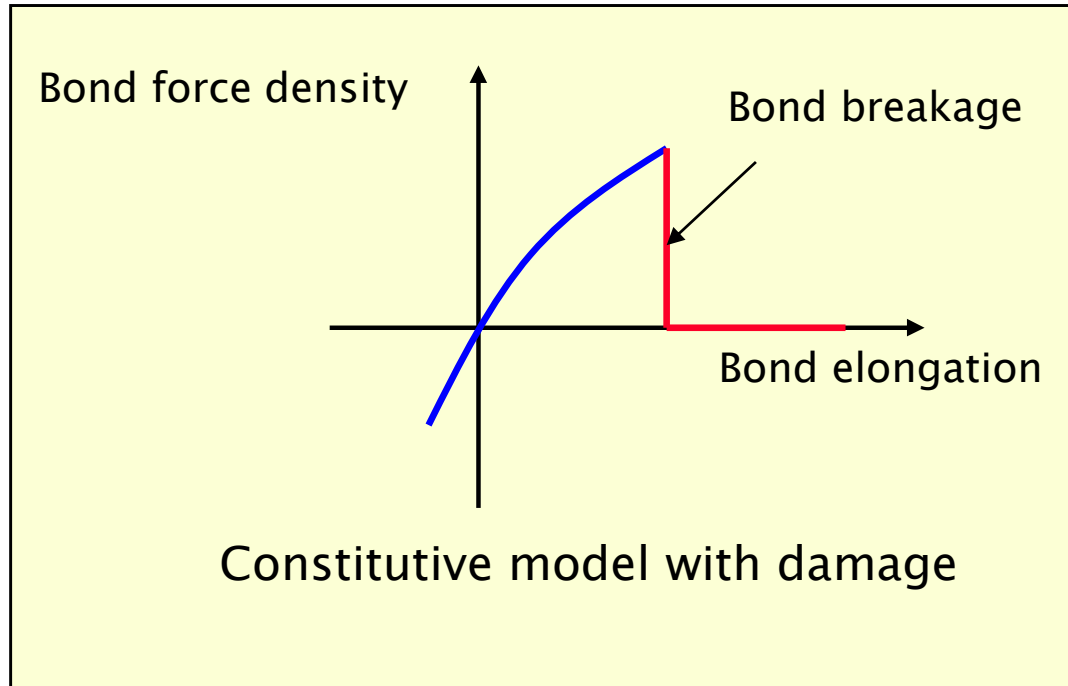
according to some *damage evolution law*:

$$\underline{\phi} = \underline{D}(\underline{\mathbf{Y}}, \underline{\dot{\mathbf{Y}}}, \dots).$$

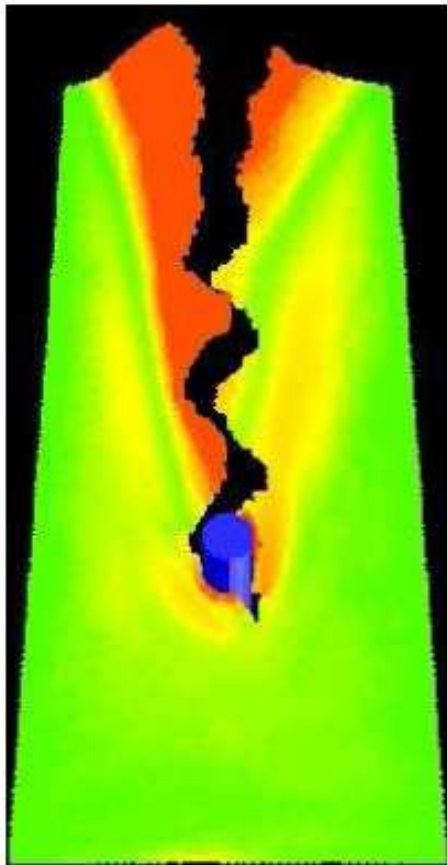
- Details of this are not important for present purposes.
- Simplest model: bond breakage.



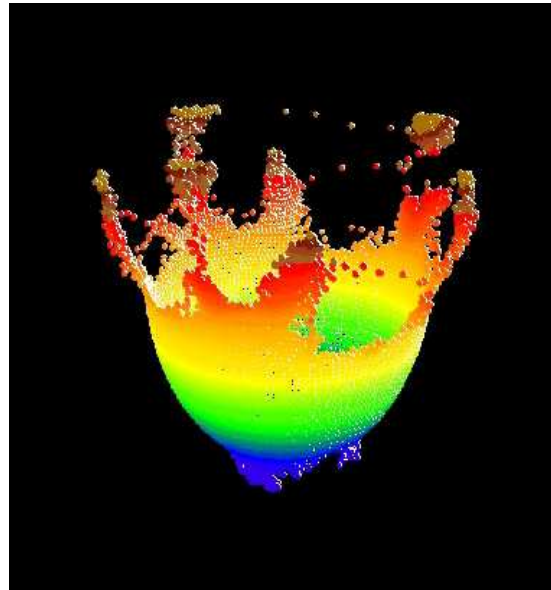
# Bond breakage and progressive failure



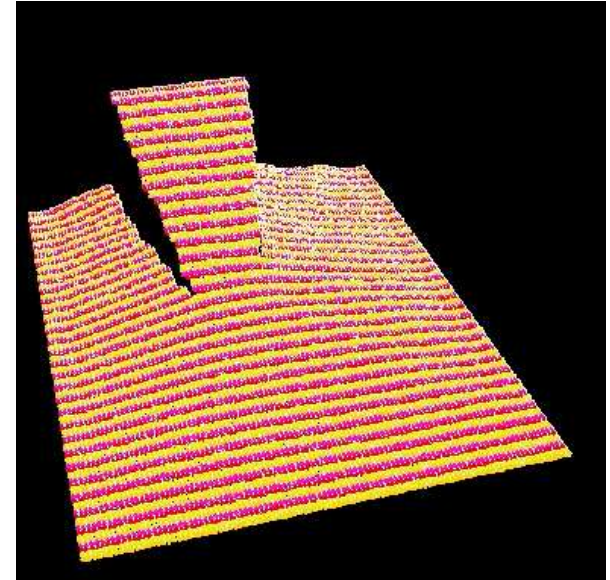
# Damage leads to fracture



Tearing instability



Balloon pop



Peeling

Main advantage of peridynamics for crack modeling

Crack growth is autonomous: same field equations apply on or off of a discontinuity.



# Entropy production and energy dissipation

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- Again using Coleman-Noll, the rate of entropy production is

$$\dot{\eta} = \frac{\dot{\psi}^d}{\theta}$$

where the *rate of energy dissipation* is given by

$$\begin{aligned}\dot{\psi}^d &= -\psi_{\underline{\phi}} \bullet \underline{\dot{\phi}} \\ &:= - \int_{\mathcal{H}} \psi_{\underline{\phi}} \langle \mathbf{x}' - \mathbf{x} \rangle \underline{\dot{\phi}} \langle \mathbf{x}' - \mathbf{x} \rangle dV'\end{aligned}$$

where  $\underline{\phi}$  is the Fréchet derivative of  $\psi$  with respect to  $\underline{\phi}$ .

- For an isothermal process, therefore

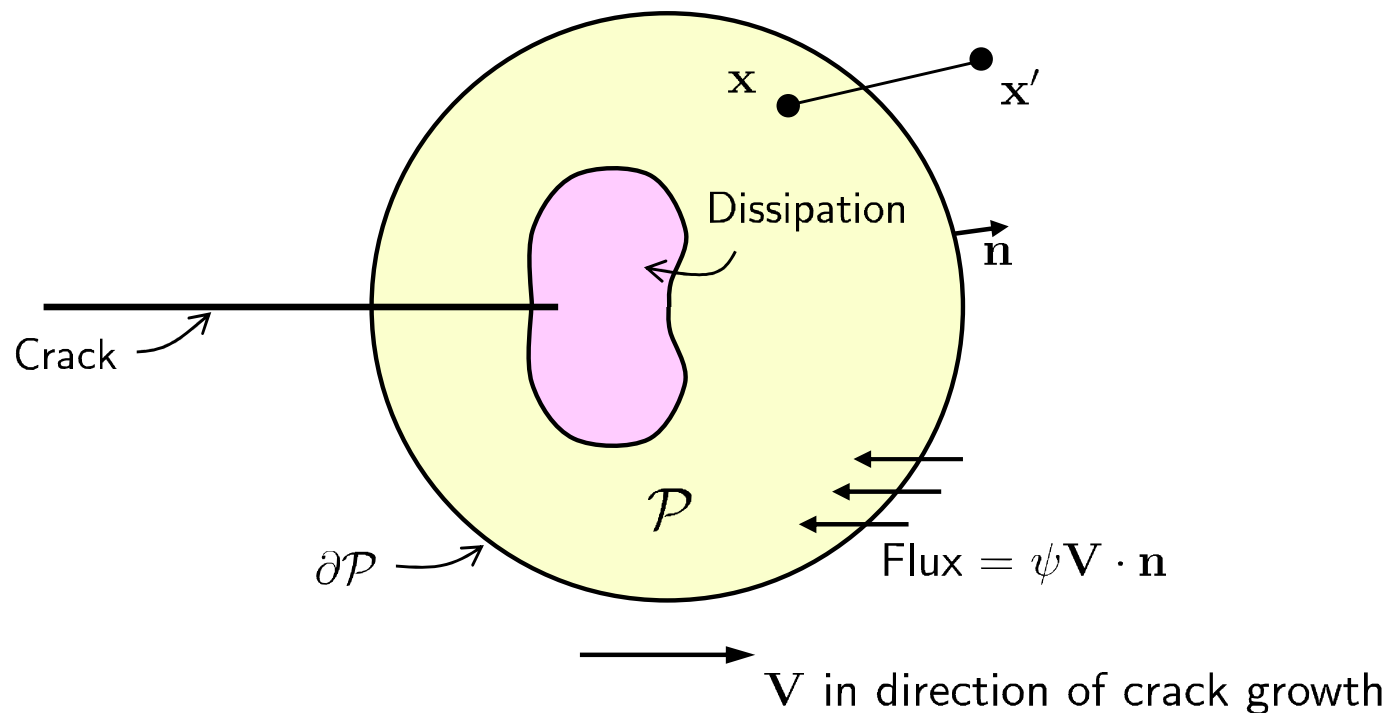
$$\dot{\psi} = \dot{\varepsilon} - \theta \dot{\eta}$$

so that

$$\dot{\psi} = \dot{\varepsilon} - \dot{\psi}^d.$$

# Analyze dissipation of energy near a defect

- Assume a homogeneous body.
- Assume a constant defect velocity .
- $\mathcal{P}$  moves with the defect through the reference configuration  $\mathcal{B}$ .

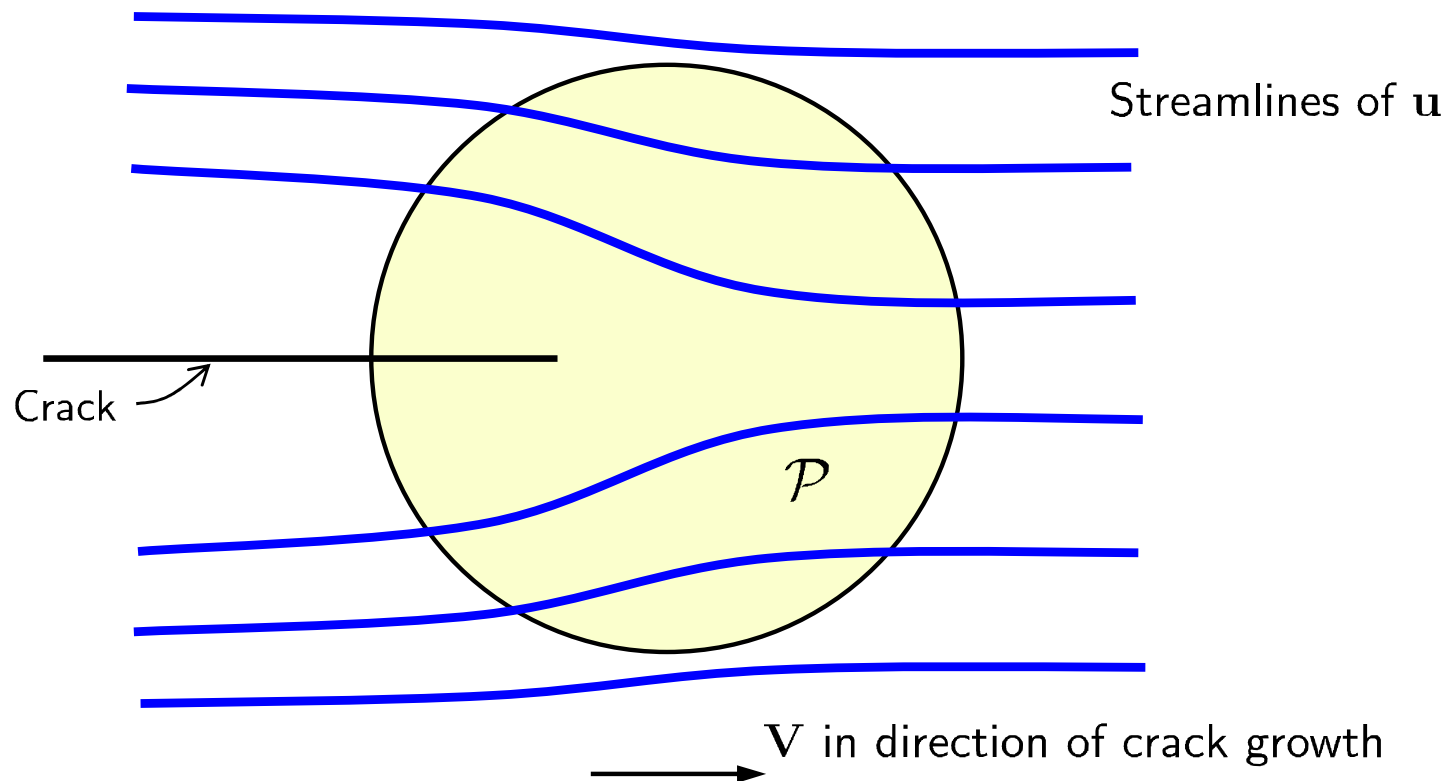


# Steady-state motion

- Assumed motion is

$$\mathbf{y}(\mathbf{x}, t) = \mathbf{x} + \mathbf{u}(\mathbf{x} - \mathbf{V}t)$$

where  $\mathbf{u}$  is a given function and  $|\mathbf{V}|$  is small.



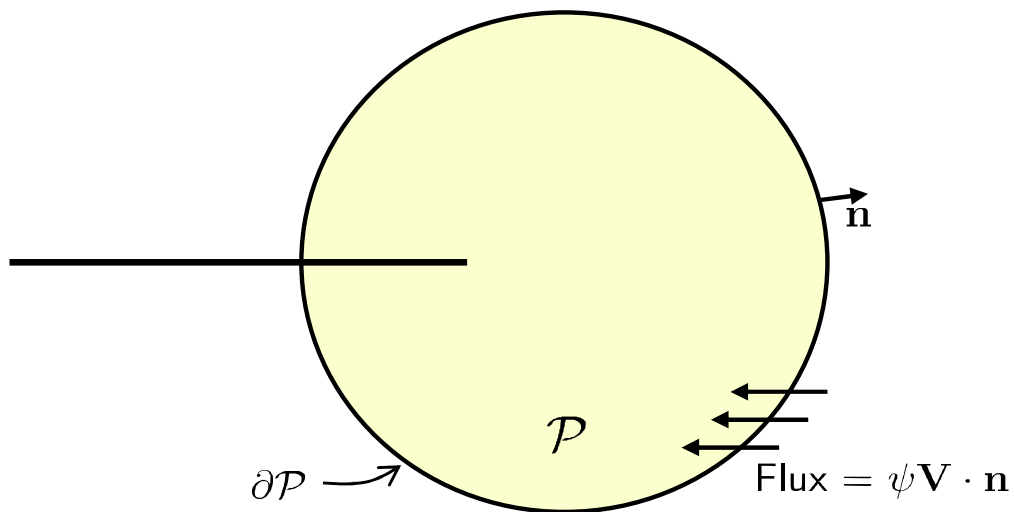
# Free energy balance

- Reynolds transport theorem implies

$$\frac{d}{dt} \int_{\mathcal{P}} \psi dV = \int_{\mathcal{P}} \dot{\psi} dV + \int_{\partial \mathcal{P}} \psi \mathbf{V} \cdot \mathbf{n} dA$$

but steady-state implies

$$\frac{d}{dt} \int_{\mathcal{P}} \psi dV = 0.$$





# Use first law to compute nonlocal work done across the boundary

- Recall

$$\dot{\psi} = \dot{\varepsilon} - \dot{\psi}^d.$$

hence

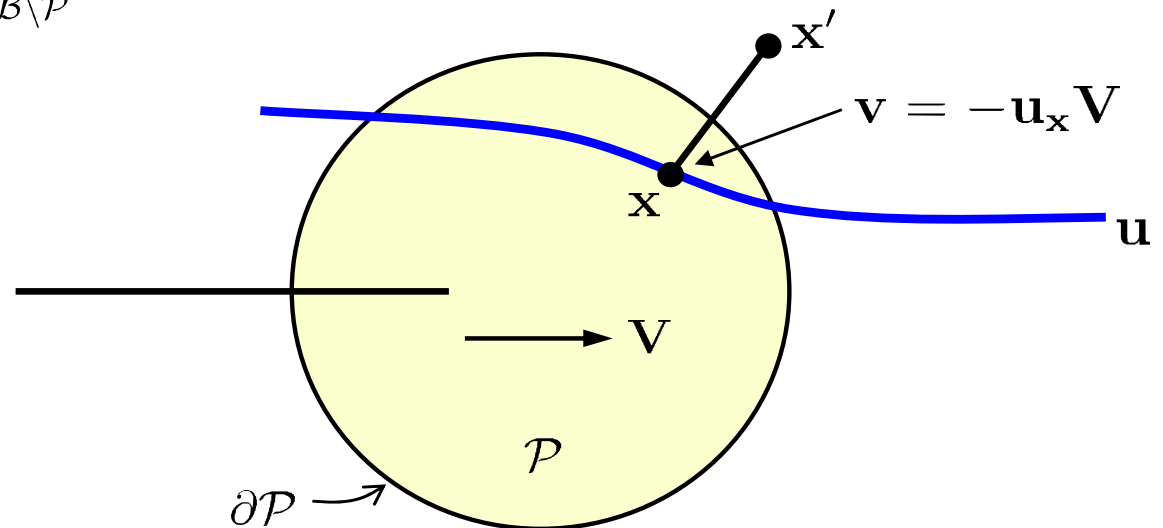
$$\int_{\mathcal{P}} (\dot{\varepsilon} - \dot{\psi}^d) dV + \int_{\partial\mathcal{P}} \psi \mathbf{V} \cdot \mathbf{n} dA = 0$$

- Global first law under present assumptions reduces to

$$\int_{\mathcal{P}} \dot{\varepsilon} dV = \int_{\mathcal{P}} \int_{\mathcal{B} \setminus \mathcal{P}} (\mathbf{t} \cdot \mathbf{v}' - \mathbf{t}' \cdot \mathbf{v}) dV' dV$$

$$\mathbf{u}_{\mathbf{x}} = \text{grad } \mathbf{u}(\mathbf{x})$$

$$\mathbf{u}'_{\mathbf{x}} = \text{grad } \mathbf{u}(\mathbf{x}')$$



# Total rate of energy dissipation

- Eliminate  $\dot{\varepsilon}$  term to find

$$\int_{\mathcal{P}} \dot{\psi}^d dV = \int_{\mathcal{P}} \int_{\mathcal{B} \setminus \mathcal{P}} (\mathbf{t} \cdot (-\mathbf{u}'_{\mathbf{x}} \mathbf{V}) - \mathbf{t}' \cdot (-\mathbf{u}_{\mathbf{x}} \mathbf{V})) dV' dV + \int_{\partial \mathcal{P}} \psi \mathbf{V} \cdot \mathbf{n} dA$$

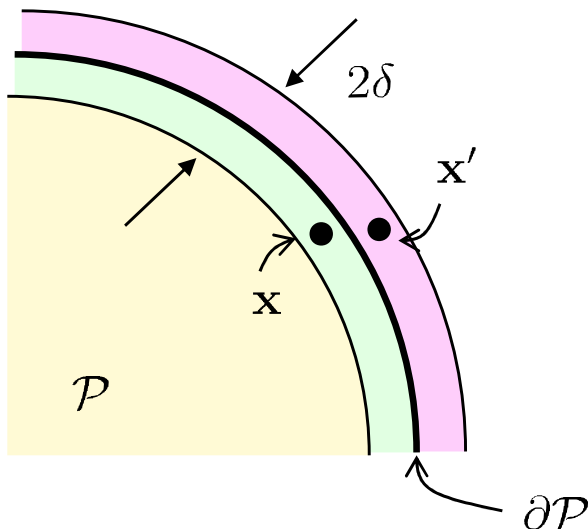
or

$$\int_{\mathcal{P}} \dot{\psi}^d dV = \mathbf{J} \cdot \mathbf{V}$$

where

$$\mathbf{J} = \int_{\mathcal{P}} \int_{\mathcal{B} \setminus \mathcal{P}} (\mathbf{u}_{\mathbf{x}}^T \mathbf{t}' - (\mathbf{u}'_{\mathbf{x}})^T \mathbf{t}) dV' dV + \int_{\partial \mathcal{P}} \psi \mathbf{n} dA$$

Peridynamic  
J-integral (3D)

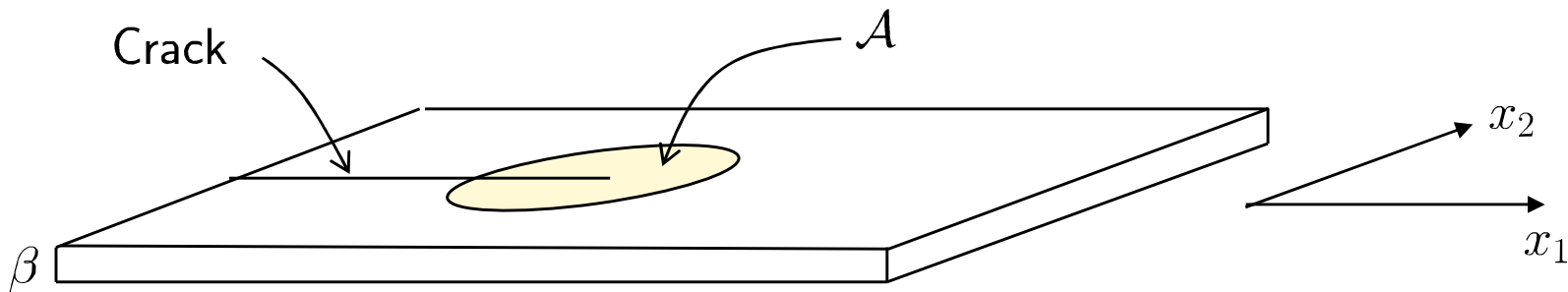


Integrand is nonzero only if  $\mathbf{x}$  and  $\mathbf{x}'$  are sufficiently close to  $\partial \mathcal{P}$ .

# Crack in a plate

- Apply to a plate of thickness  $\beta$ .  $\mathcal{A}$  is the interior of a curve in the plane.
- Assume crack grows in the  $x_1$  direction.

$$J_1 = \beta^2 \int_{\mathcal{A}} \int_{\mathcal{B} \setminus \mathcal{A}} \left( \frac{\partial \mathbf{u}}{\partial x_1} \cdot \mathbf{t}' - \frac{\partial \mathbf{u}'}{\partial x_1} \cdot \mathbf{t} \right) dA' dA + \beta \int_{\partial \mathcal{A}} \psi n_2 ds$$





# Crack in a plate: Limit of small horizon

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- Small horizon:

$$\frac{\partial \mathbf{u}}{\partial x_1} \approx \frac{\partial \mathbf{u}'}{\partial x_1}$$

hence

$$\begin{aligned} J_1 &\approx \beta^2 \int_{\mathcal{A}} \frac{\partial \mathbf{u}}{\partial x_1} \cdot \left[ \int_{\mathcal{B} \setminus \mathcal{A}} (\mathbf{t}' - \mathbf{t}) \, dA' \right] dA + \beta \int_{\partial \mathcal{A}} \psi n_2 \, ds \\ &= \beta \int_{\partial \mathcal{A}} \left[ -\frac{\partial \mathbf{u}}{\partial x_1} \cdot \boldsymbol{\tau} \, ds + \psi n_2 \right] ds \end{aligned}$$

where  $\boldsymbol{\tau}$  is the traction vector on  $\partial \mathcal{A}$ .

- This is the same as Rice's  $J$ -integral in the standard theory (except for factor of  $\beta$ ).



# Summary

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$$\mathbf{J} = \int_{\mathcal{P}} \int_{\mathcal{B} \setminus \mathcal{P}} (\mathbf{u}_{\mathbf{x}}^T \mathbf{t}' - (\mathbf{u}'_{\mathbf{x}})^T \mathbf{t}) dV' dV + \int_{\partial \mathcal{P}} \psi \mathbf{n} dA$$

- Directly computed the free energy dissipated by a defect based on the first law and on steady-state assumptions.
- Did not need to assume anything about the physical dissipative mechanism.
- Did not assume that dissipation is confined to a small process zone.
- Defect may or may not involve a discontinuity in  $\mathbf{u}$  (consistent with the “spirit of peridynamics”).
- For more info: SS & RL, “Peridynamic Theory of Solid Mechanics,” to appear in *Advances in Applied Mechanics*, vol. 44 (2010).